THE UNUSUAL VERTICAL MASS DISTRIBUTION OF NGC 4013 SEEN THROUGH THE SPITZER SURVEY OF STELLAR STRUCTURE IN GALAXIES (S⁴G)

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ABSTRACT

NGC 4013 is a nearby Sb edge-on galaxy known for its "prodigious" H I warp and its "giant" tidal stream. Previous work on this unusual object shows that it cannot be fitted satisfactorily by a canonical thin+thick disk structure. We have produced a new decomposition of NGC 4013, considering three stellar flattened components (thin+thick disk plus an extra and more extended component) and one gaseous disk. All four components are considered to be gravitationally coupled and isothermal. To do so, we have used the 3.6 μ m images from the *Spitzer* Survey of Stellar Structure in Galaxies. We find evidence for NGC 4013 indeed having a thin and a thick disk and an extra flattened component. This smooth and extended component (scale height $z_{EC} \sim 3$ kpc) could be interpreted as a thick disk or as a squashed ellipsoidal halo and contains ~20% of the total mass of all three stellar components. We argue it is unlikely to be related to the ongoing merger or due to the off-plane stars from a warp in the other two disk components. Instead, we favor a scenario in which the thick disk and the extended component were formed in a two-stage process, in which an initially thick disk has been dynamically heated by a merger soon enough in the galaxy history to have a new thick disk formed within it.

Key words: galaxies: individual (NGC 4013) – galaxies: photometry – galaxies: spiral – galaxies: structure

Online-only material: color figure

1. INTRODUCTION

Thick disks, first detected by Burstein (1979) and Tsikoudi (1979), are seen in edge-on galaxies as excesses of light a few thin disk scale heights above the galaxy midplanes. They are known to be ubiquitous (Yoachim & Dalcanton 2006; Comerón et al. 2011a) and their properties give important clues for understanding galaxy formation and evolution (Comerón et al. 2011b, hereafter CO11b and references therein). Recent studies (Robertson et al. 2006; Elmegreen & Elmegreen 2006; Brook et al. 2007; Richard et al. 2010) suggest an in situ formation mechanism for a significant fraction of the thick disk mass. This was recently supported further by our result that the masses of thick and thin disks are of the same order (CO11b). Other formation mechanisms such as disk kinematical heating due to its own overdensities (Villumsen 1985; Hänninen & Flynn 2002; Schönrich & Binney 2009; Bournaud et al. 2009) and the accretion of stars from infalling satellites (Statler 1988; Gilmore et al. 2002; Abadi et al. 2003; Navarro et al. 2004; Martin et al.

2004; Read et al. 2008) also contribute to the thick disk mass (CO11b).

In CO11b we made thin+thick disk decompositions of 46 edge-on galaxies using images from the *Spitzer* Survey of Stellar Structure in Galaxies (S⁴G; Sheth et al. 2010). However, two galaxies, ESO 079-003 and NGC 4013, could not be successfully fitted down to low surface brightness due to the presence of an extra light component not accounted for in our fits (affecting significantly the luminosity profiles starting at $\mu_{3.6\,\mu\text{m}}(AB) = 23 \text{ mag arcsec}^{-2}$). In CO11b, NGC 3628 also presents an obvious third component, but at a lower surface brightness ($\mu_{3.6\,\mu\text{m}}(AB) = 24.5 \text{ mag arcsec}^{-2}$). The aim of this Letter is to study the properties of these extra components. As ESO 079-003 is located near a bright star, which makes its study at low surface brightness levels difficult, and NGC 3628 presents a disturbed morphology due to a recent interaction we focused on NGC 4013.

NGC 4013 is an Sb galaxy (Buta et al. 2007), at 18.6 ± 2.5 Mpc (NED average for 13 redshift-independent

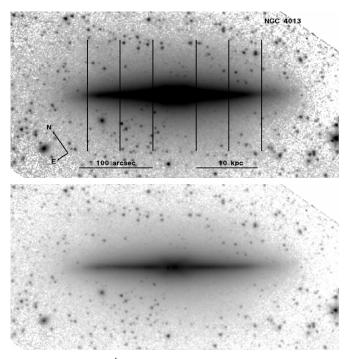


Figure 1. 3.6 μ m band S⁴G image of NGC 4013 with two different luminosity stretches. The vertical lines indicate the limits of the bins for which luminosity profiles have been produced, from left to right, at galactocentric distances of $-0.8 r_{25} < R < -0.5 r_{25}, -0.5 r_{25} < R < -0.2 r_{25}, -0.2 r_{25} < R < 0.2 r_{25}, 0.2 r_{25} < R < 0.5 r_{25}, and 0.5 r_{25} < R < 0.8 r_{25}$. In order to avoid the influence of the bulge we have not produced fits for the central bin.

measurements). Its optical diameter is $D_{25} = 294''$ (Hyper-LEDA; Paturel et al. 2003). It is often described using superlative adjectives: it has a "prodigious" H I warp (Bottema et al. 1987; Bottema 1995, 1996) and a "giant" stellar tidal stream with an age of a few Gyr (Martínez-Delgado et al. 2009, hereafter MD09). The H I warp starts just at the optical edge of the galaxy (Bottema 1995) and it is one of the largest warps ever observed. It may have been triggered by the minor merger event which caused the tidal stream (MD09). In addition, NGC 4013 has a boxy bulge (Jarvis 1986) which could be tracing an edge-on bar (Athanassoula & Misiriotis 2002; Martínez-Valpuesta et al. 2006) or be the consequence of a merging event (Binney & Petrou 1985).

The S⁴G 3.6 μ m band image used for the study presented in this Letter is shown in Figure 1.

2. FITTING PROCEDURE

In CO11b, the observed luminosity profiles were fitted with synthetic profiles resulting from coupling two stellar plus one gaseous isothermal disks (using the equations in Narayan & Jog 2002). The solutions are not analytic, so the fit was done by comparing the luminosity profile to a grid of pre-computed models with different thick-to-thin central mass density ratios (ρ_{T0}/ρ_{t0}) and thick-to-thin velocity dispersions in the vertical direction ratios (σ_T/σ_t), where "T" stands for the thick disk and "t" stands for the thin disk. Both observed luminosity and pre-computed profiles were scaled to have a midplane luminosity equal to unity and have $\rho(z = 200)/\rho(z = 0) = 0.1$. In addition the synthetic profiles were convolved with a Gaussian kernel with a full width at half-maximum (FWHM) equal to 2."2 in order to account for the point-spread function of the 3.6 μ m band image (S⁴G "super-PSF"; Sheth et al. 2010). The mass-to-light

ratios (Y) for both thin and thick disk stars had to be assumed in order to make the computation of the grid of models, and reasonable limiting cases with $\Upsilon_T/\Upsilon_t = 1.2$ and $\Upsilon_T/\Upsilon_t = 2.4$ were studied (see CO11b). The gaseous disk was assumed to have a column mass density equal to 20% of that of the thin disk. The case without gas was also studied yielding similar results to the with-gas case, but the fit quality was slightly worse.

The fits were made ignoring the midplane pixel and over a range of magnitudes, Δm , which was defined as the range for which either the square root of the χ^2 of the fit was smaller than $\sqrt{\chi^2} < 0.1 \text{ mag arcsec}^{-2}$ or down to a limiting magnitude $\mu_1(AB) = 26 \text{ mag arcsec}^{-2}$. The discussion on how we chose this goodness-of-fit parameter and this limiting magnitude appear in CO11b.

In CO11b, for the NGC 4013 luminosity profiles at $0.2r_{25} < |R| < 0.5r_{25}$ the fits could only be performed down to μ (AB) ~ 23 mag arcsec⁻², at which point our criterion for the quality of the fit, $\sqrt{\chi^2} > 0.1$ mag arcsec⁻², was not met. The reason for that was the presence of a third component which made our two stellar disk decomposition insufficient at describing NGC 4013. This component was called "halo" by van der Kruit & Searle (1982) and by MD09 who reported that it is box-shaped (although the boxiness is probably caused by the location of the tidal streams and not by the intrinsic shape of the component).

We adapted the code used in C011b to include a third component in equilibrium with the two stellar disks and the gaseous disk. This is a natural approach because the luminosity profile decays exponentially with height once in the range of heights for which the more extended component dominates, and because the solution of the equations for a set of coupled flattened components can be approximated as exponential at high distances above the midplane. However, the fact of adding a third flattened component does not imply that it is a disk; this is because, without kinematical information, a squashed ellipsoidal halo nature for this component cannot be discarded. Arguments in favor of this component being a disk are (1) its relatively high surface brightness and (2) its luminosity profile parallel to the midplane direction (not shown here) which is that of a typical edge-on disk, with a shallow slope for low R and an exponential slope at larger R. Arguments in favor of the extended component being an squashed elliptical halo are (1) its isophotes are not disky (MD09) and may be very close to elliptical if the light of the tidal streams could be removed and (2) its ellipticity $(\epsilon = 0.63$ when measured in an ellipse fit between radius 120'', which is the truncation radius of the thin disk, and 170'', where the extended component starts to be highly affected by noise) is compatible with that of simulated elliptical haloes (see, e.g., Lee et al. 2005). Due to its uncertain nature we will hereafter term this component as "extended component" (EC).

The grid of models we used for the fits had ρ_{T0}/ρ_{t0} , ρ_{T0}/ρ_{EC0} , σ_T/σ_t , and σ_T/σ_{EC} as free parameters, where EC denotes the extended component. Our grid of models has been computed including a gaseous disk and using the same normalizations as in CO11b. We considered the cases $\Upsilon_T/\Upsilon_t = 1.2$ and $\Upsilon_T/\Upsilon_t = 2.4$. In both cases we set $\Upsilon_T/\Upsilon_{EC} = 1.0$. This is justified by the fact that once above the midplane dust lane (z > 10'', a region mainly influenced by the thick disk and the EC), the colors remain roughly constant, as can be seen in Figure 2. Figure 2 provides extra evidence that the thick disk and the EC contain old star populations since the average color for z > 10'' is $\overline{g' - r'(z > 10'')} = 0.73$ mag, which is compatible with the average colors predicted for S0 galaxies (g' - r' = 0.68 mag;

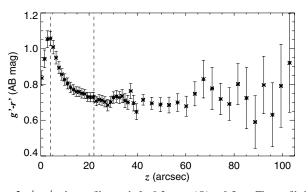


Figure 2. g' - r' color profiles made for $0.2r_{25} < |R| < 0.5r_{25}$. The profile has been produced using Sloan Digital Sky Survey Data Release 7 data (Abazajian et al. 2009). Points for $z \leq 40''$ are calculated every three pixels ($\sim 1''_{.2}$) and those with z > 40'' are calculated every nine pixels ($\sim 3''_{.6}$). The error bars represent the 2σ statistical errors. The vertical lines separate the regions dominated by the luminosity of the thin disk, the thick disk, and the EC for $\Upsilon_T/\Upsilon_t = 1.2$.

Fukugita et al. 1995). The reddening for z < 10'' is caused by the midplane dust lane. Since we found no significant influence of this midplane dust on the 3.6 μ m band profile for this galaxy in CO11b, we considered the midplane dust lane to have no effect on our fits.

3. RESULTS

The addition of a third stellar component allows us to fit the surface brightness profile down to $\mu(AB) = 26.0 \text{ mag arcsec}^{-2}$. The fit is significantly better than that published in CO11b (Figure 3 and Table 1) in the sense that it goes far deeper. The fact that for $0.2r_{25} < |R| < 0.5r_{25} \Delta m$ is 3.0 mag arcsec⁻² larger than what was achieved in CO11b and that the outermost fitted

z goes from 25''-45'' in CO11b to 70''-100'' in the present work argues for the correctness of the fit, and thus for the physical reality of the third component. The numbers exclude a possible alternative, namely that the better fit is achieved merely by the addition of more free parameters.

The fitted properties of the thin and the thick disk are fairly similar to those reported in CO11b (Table 1), and the ratio of the column mass densities Σ_T/Σ_t is equal, within 10%, to that obtained for the three bins for which we succeeded to obtain a fit in CO11b. The midplane stellar densities are not much affected by the inclusion of the EC, and its main effect is to reduce the scale heights of the thin and thick disks. The small effect introduced by the EC in Σ_T/Σ_t is due to the fact that the midplane density of the EC is ~ 10 (~ 10) times smaller than that of the thick disk and ~ 20 (~ 10) times smaller than that of the thin disk for $\Upsilon_T/\Upsilon_t = 1.2$ ($\Upsilon_T/\Upsilon_t = 2.4$). The fact that possible undetected ECs do not have much influence on the results in CO11b shows the robustness of our fitting approach in general.

Each of the three stellar components has a significant range in vertical height for which it dominates the luminosity profile, making it easy to determine its properties and degeneracies unlikely. The thin disk luminosity dominates for z < 5'', the thick disk dominates for 5'' < z < 20'', and the EC dominates for z > 20''. The only problem in the fit is that the thin disk scale height is poorly constrained due to poor sampling (z_t is around 1...5, which is smaller than the FWHM).

The EC, if considered to be a disk, has an exceptionally large scale height, $z_{\rm EC} \sim 3$ kpc, comparable only to that of thick disks in NGC 0678, NGC 4437, and NGC 4565 in CO11b. The scale height is significantly larger for the $-0.8 r_{25} < R < -0.5 r_{25}$ bin probably because its luminosity profile is affected by the brightest loop of the tidal stream (MD09). The $\rho_{\rm T0}/\rho_{\rm EC0}$ ratio

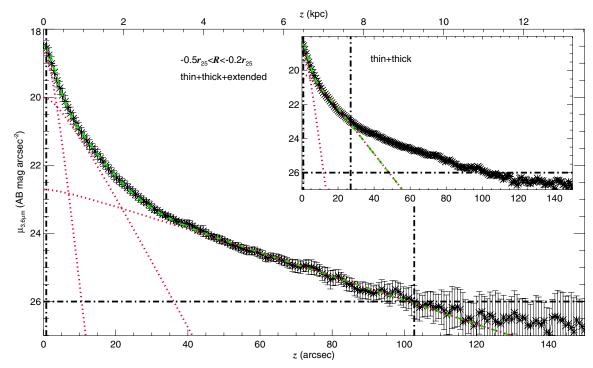


Figure 3. Example of a fit to the vertical luminosity profiles of NGC 4013 considering $\Upsilon_T/\Upsilon_t = 1.2$. Data points with error bars (2σ statistical errors) represent the observed luminosity profile, and the dashed green curve the best fit. The dotted red curves indicate the contributions of the three stellar components. The dash-dotted vertical lines indicate the limits of the range in vertical distance above the midplane used for the fit. The horizontal line represents the $\mu(AB) = 26.0$ mag arcsec⁻² level down to which the fits have been done. The inset shows the thin+thick disk best fit obtained for NGC 4013 in CO11b. (A color version of this figure is available in the online journal.)

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$ \begin{array}{c c} \mbox{Fitting Range} & \mbox{Y}_{\rm T}/\mbox{Y}_{\rm t} = 1.2 & \mbox{Y}_{\rm T}/\mbox{Y}_{\rm t} = 2.4 \\ \hline -0.8 r_{25} < R < -0.5 r_{25} & \mbox{μ_1} = 25.96 \mbox{mag arcsec}^{-2} \\ \Delta m = 6.0 \mbox{mag arcsec}^{-2} \\ \rho_{\rm TO}/\rho_{0} = 0.35 & \mbox{$\rho_{\rm TO}}/\rho_{\rm DC} = 0.64 \\ \rho_{\rm TO}/\rho_{\rm EC0} = 7.00 & \mbox{$\rho_{\rm TO}}/\rho_{\rm EC} = 0.38 \\ \mbox{$\sigma_{\rm T}/\sigma_{\rm EC}$} = 0.38 & \mbox{$\sigma_{\rm T}/\sigma_{\rm EC}$} = 0.38 \\ \mbox{$\sigma_{\rm T}/\sigma_{\rm EC}$} = 0.38 & \mbox{$\sigma_{\rm T}/\sigma_{\rm EC}$} = 0.38 \\ \mbox{$\Sigma_{\rm T}/\Sigma_{\rm Ec}$} = 1.21 & \mbox{$\Sigma_{\rm T}/\Sigma_{\rm Ec}$} = 1.20 \mbox{$pc$} \\ \mbox{$z_{\rm T}$} = 610 \mbox{$pc$} & \mbox{$z_{\rm T}$} = 120 \mbox{$pc$} \\ \mbox{$z_{\rm T}$} = 610 \mbox{$pc$} & \mbox{$z_{\rm T}$} = 2.50 \mbox{$pm ag arcsec}^{-2} \\ \mbox{$\rho_{\rm TO}/\rho_{00}$} = 0.36 & \mbox{$\rho_{\rm TO}/\rho_{00}$} = 0.60 \\ \mbox{$\rho_{\rm TO}/\rho_{\rm EC0}$} = 12.00 & \mbox{$\rho_{\rm TO}/\rho_{\rm EC0}$} = 12.00 \\ \mbox{$\rho_{\rm TO}/\rho_{\rm EC0}$} = 12.00 & \mbox{$\rho_{\rm TO}/\rho_{\rm EC0}$} = 12.00 \\ \mbox{$\sigma_{\rm T}/\sigma_{\rm t}$} = 2.45 & \mbox{$\sigma_{\rm T}/\sigma_{\rm t}$} = 2.69 \\ \mbox{$\sigma_{\rm T}/\sigma_{\rm t}$} = 2.45 & \mbox{$\sigma_{\rm T}/\sigma_{\rm t}$} = 2.69 \\ \mbox{$\sigma_{\rm T}/\sigma_{\rm t}$} = 2.45 & \mbox{$\sigma_{\rm T}/\sigma_{\rm t}$} = 2.69 \\ \mbox{$\sigma_{\rm T}/\sigma_{\rm t}$} = 2.45 & \mbox{$\sigma_{\rm T}/\sigma_{\rm t}$} = 2.69 \\ \mbox{$\sigma_{\rm T}/\sigma_{\rm t}$} = 2.91 & \mbox{$\Sigma_{\rm T}/\Sigma_{\rm EC}$} = 3.10 \ \mbox{$pc$} & \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $		Table 1Result of the Fits	
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$ \begin{array}{c} \sigma_{\rm T}/\sigma_{\rm EC}=0.38 & \sigma_{\rm T}/\sigma_{\rm EC}=0.38 \\ \Sigma_{\rm T}/\Sigma_{\rm t}=1.21 & \Sigma_{\rm T}/\Sigma_{\rm t}=2.23 \\ \Sigma_{\rm T}/\Sigma_{\rm EC}=1.54 & \Sigma_{\rm T}/\Sigma_{\rm EC}=1.46 \\ z_{\rm t}=130 \ {\rm pc} & z_{\rm t}=120 \ {\rm pc} \\ z_{\rm T}=610 \ {\rm pc} & z_{\rm T}=580 \ {\rm pc} \\ z_{\rm EC}=3660 \ {\rm pc} & z_{\rm EC}=3500 \ {\rm pc} \\ z_{\rm EC}=3600 \ {\rm pc} & z_{\rm EC}=3500 \ {\rm pc} \\ \end{array} \right. \\ \hline -0.5 r_{25} < R < -0.2 r_{25} & \mu_{\rm I}=25.99 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m=7.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m=5.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m=5.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m=5.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m=5.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m=5.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m=5.5 \ {\rm mg} \ {\rm arcsec}^{-2} \\ \Delta m=5.5 \ {\rm mg} \ {\rm arcsec}^{-2} \\ \Delta m=5.5 \ {\rm mg} \ {\rm arc$			
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$\begin{split} & \sum_{T} / \sum_{EC} = 1.54 \qquad \sum_{T} / \sum_{EC} = 1.46 \\ z_t = 130 \ \text{pc} & z_T = 580 \ \text{pc} \\ z_{EC} = 3660 \ \text{pc} & z_{EC} = 3500 \ \text{pc} \\ \hline \\ \hline \\ -0.5 r_{25} < R < -0.2 r_{25} \qquad & \mu_1 = 25.99 \ \text{mag} \ \text{arcsec}^{-2} \\ \Delta m = 7.5 \ \text{mag} \ \text{arcsec}^{-2} \\ \Delta m = 7.5 \ \text{mag} \ \text{arcsec}^{-2} \\ \Delta m = 7.5 \ \text{mag} \ \text{arcsec}^{-2} \\ \rho_{TO} / \rho_{0} = 0.36 \qquad \rho_{TO} / \rho_{0} = 0.60 \\ \rho_{TO} / \rho_{EC0} = 12.00 \qquad \rho_{TO} / \rho_{EC0} = 12.00 \\ \sigma_{T} / \sigma_{EC} = 0.41 \qquad \sigma_{T} / \sigma_{EC} = 0.41 \\ \Sigma_{T} / \Sigma_{t} = 2.13 \\ \Sigma_{T} / \Sigma_{EC} = 2.91 \qquad \Sigma_{T} / \Sigma_{EC} = 3.02 \\ z_t = 110 \ \text{pc} \qquad z_t = 510 \ \text{pc} \qquad z_{T} = 530 \ \text{pc} \\ z_{EC} = 2780 \ \text{pc} \qquad z_{EC} = 2890 \ \text{pc} \\ \hline \\ 0.2 r_{25} < R < 0.5 r_{25} \qquad \mu_1 = 25.93 \ \text{mag} \ \text{arcsec}^{-2} \\ \rho_{TO} / \rho_{0} = 0.35 \qquad \rho_{TO} / \rho_{0} = 0.64 \\ \rho_{TO} / \rho_{EC0} = 11.60 \qquad \rho_{TO} / \rho_{EC0} = 10.60 \\ \sigma_{T} / \sigma_{t} = 2.60 \qquad \sigma_{T} / \sigma_{t} = 2.69 \\ \sigma_{T} / \sigma_{EC} = 0.44 \qquad \sigma_{T} / \sigma_{EC} = 0.43 \\ \Sigma_{T} / \Sigma_{EC} = 3.13 \qquad \Sigma_{T} / \Sigma_{EC} = 2.94 \\ z_t = 110 \ \text{pc} \qquad z_t = 100 \ \text{pc} \\ z_T = 520 \ \text{pc} \qquad z_T = 500 \ \text{pc} \\ z_{EC} = 2540 \ \text{pc} \qquad z_{EC} = 2470 \ \text{pc} \\ \hline \\ 0.5 r_{25} < R < 0.8 r_{25} \qquad \mu_1 = 25.67 \ \text{mag} \ \text{arcsec}^{-2} \\ \rho_{TO} / \rho_{0} = 0.39 \qquad \rho_{TO} / \rho_{0} = 0.70 \\ \rho_{TO} / \rho_{EC0} = 5.57 \qquad \rho_{TO} / \rho_{EC} = 5.00 \ \sigma_{T} / \sigma_{t} = 2.30 \\ \sigma_{T} / \sigma_{EC} = 0.44 \qquad \sigma_{T} / \sigma_{EC} = 0.44 \\ \Sigma_{T} / \Sigma_{EC} = 1.19 \qquad \Sigma_{T} / \Sigma_{EC} = 0.44 \\ \Sigma_{T} / \Sigma_{EC} = 1.19 \qquad \rho_{TO} / \rho_{EC0} = 5.00 \ \sigma_{T} / \sigma_{t} = 2.30 \ \sigma_{T} / \sigma_{t} = 2.30 \ \sigma_{T} / \sigma_{t} = 2.35 \ \sigma_{T} / \sigma_{t} = 2.50 \ \sigma_{T} / \sigma_{t} = 2.35 \ \sigma_{T} / \sigma_{t} = 2.50 \ \sigma_{T} / \sigma_{t} = 2.35 \ \sigma_{T} / \sigma_{t} = 2.50 \ \sigma_{T} / \sigma_{t} = 2.50 \ \sigma_{T} / \sigma_{t} = 2.35 \ \sigma_{T} / \sigma_{t} = 2.50 \ \sigma_{T} / \sigma_{T} / \sigma_{t} = 2.50 \ \sigma_{T} $			
$ \begin{array}{c} z_{\rm t} = 130 \ {\rm pc} & z_{\rm t} = 120 \ {\rm pc} \\ z_{\rm T} = 610 \ {\rm pc} & z_{\rm T} = 580 \ {\rm pc} \\ z_{\rm EC} = 3660 \ {\rm pc} & z_{\rm EC} = 3500 \ {\rm pc} \\ \hline \end{array} \\ \hline \begin{array}{c} -0.5 r_{25} < R < -0.2 r_{25} \\ \hline \end{array} \\ \begin{array}{c} \mu_1 = 25.99 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 7.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \rho_{\rm T0}/\rho_{0} = 0.36 & \rho_{\rm T0}/\rho_{0} = 0.60 \\ \rho_{\rm T0}/\rho_{\rm EC0} = 12.00 & \rho_{\rm T0}/\rho_{\rm EC0} = 12.00 \\ \sigma_{\rm T}/\sigma_{\rm EC} = 0.41 & \sigma_{\rm T}/\sigma_{\rm EC} = 0.41 \\ \Sigma_{\rm T}/\Sigma_{\rm E} = 2.91 & \Sigma_{\rm T}/\Sigma_{\rm EC} = 3.02 \\ z_{\rm t} = 110 \ {\rm pc} & z_{\rm t} = 110 \ {\rm pc} \\ z_{\rm T} = 510 \ {\rm pc} & z_{\rm T} = 530 \ {\rm pc} \\ z_{\rm EC} = 2780 \ {\rm pc} & z_{\rm EC} = 2890 \ {\rm pc} \\ \hline \end{array} \\ \hline \begin{array}{c} 0.2 r_{25} < R < 0.5 r_{25} \\ \hline \end{array} \\ \begin{array}{c} \mu_1 = 25.93 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 7.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 7.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 7.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 7.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 7.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 7.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \rho_{\rm T0}/\rho_{0} = 0.35 & \rho_{\rm T0}/\rho_{0} = 0.64 \\ \rho_{\rm T0}/\rho_{\rm EC0} = 11.60 & \rho_{\rm T0}/\rho_{\rm EC0} = 10.60 \\ \sigma_{\rm T}/\sigma_{\rm t} = 2.69 \\ \sigma_{\rm T}/\sigma_{\rm EC} = 0.44 & \sigma_{\rm T}/\sigma_{\rm EC} = 0.43 \\ \Sigma_{\rm T}/\Sigma_{\rm E} = 3.13 & \Sigma_{\rm T}/\Sigma_{\rm E} = 2.25 \\ \Sigma_{\rm T}/\Sigma_{\rm EC} = 3.13 & \Sigma_{\rm T}/\Sigma_{\rm E} = 2.94 \\ z_{\rm t} = 110 \ {\rm pc} & z_{\rm t} = 100 \ {\rm pc} \\ z_{\rm T} = 520 \ {\rm pc} & z_{\rm T} = 500 \ {\rm pc} \\ z_{\rm EC} = 2540 \ {\rm pc} & z_{\rm EC} = 2470 \ {\rm pc} \\ \hline \end{array} \\ \hline 0.5 r_{25} < R < 0.8 r_{25} & \mu_1 = 25.67 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 5.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 5.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \rho_{\rm T0}/\rho_{0} = 0.39 & \rho_{\rm T0}/\rho_{0} = 0.70 \\ \sigma_{\rm T}/\sigma_{\rm EC} = 0.44 & \sigma_{\rm T}/\sigma_{\rm EC} = 0.44 \\ \Sigma_{\rm T}/\Sigma_{\rm E} = 1.19 & \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.48 \\ z_{\rm T}/\Sigma_{\rm E} = 1.58 & \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.48 \\ z_{\rm T}/\Sigma_{\rm E} = 1.58 & \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.48 \\ z_{\rm T}/\Sigma_{\rm E} = 1.59 \ {\rm pc} & z_{\rm T} = 550 \ {\rm pc} \\ z_{\rm T} = 620 \ {\rm pc} & z_{\rm T} = 550 \ {\rm pc} \\ \end{array} $		-, -	-, -
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$\frac{z_{\rm EC} = 3660 \ {\rm pc}}{1-0.5 r_{25} < R < -0.2 r_{25}} \qquad \begin{array}{c} \mu_1 = 25.99 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 7.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 7.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \rho_{\rm T0}/\rho_{\rm EC0} = 12.00 \qquad \rho_{\rm T0}/\rho_{\rm EC0} = 12.00 \\ \sigma_{\rm T}/\sigma_{\rm t} = 2.45 \qquad \sigma_{\rm T}/\sigma_{\rm t} = 2.69 \\ \sigma_{\rm T}/\sigma_{\rm EC} = 0.41 \qquad \sigma_{\rm T}/\sigma_{\rm EC} = 0.41 \\ \Sigma_{\rm T}/\Sigma_{\rm t} = 1.19 \qquad \Sigma_{\rm T}/\Sigma_{\rm EC} = 3.02 \\ z_{\rm t} = 110 \ {\rm pc} \qquad z_{\rm T} = 510 \ {\rm pc} \qquad z_{\rm T} = 510 \ {\rm pc} \\ z_{\rm T} = 510 \ {\rm pc} \qquad z_{\rm T} = 510 \ {\rm pc} \qquad z_{\rm EC} = 2890 \ {\rm pc} \\ 0.2 r_{25} < R < 0.5 r_{25} \qquad \mu_1 = 25.93 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \rho_{\rm T0}/\rho_{\rm 00} = 0.35 \qquad \rho_{\rm T0}/\rho_{\rm 00} = 0.64 \\ \rho_{\rm T0}/\rho_{\rm EC0} = 11.60 \qquad \rho_{\rm T0}/\rho_{\rm EC0} = 10.60 \\ \sigma_{\rm T}/\sigma_{\rm EC} = 0.44 \qquad \sigma_{\rm T}/\sigma_{\rm EC} = 0.43 \\ \Sigma_{\rm T}/\Sigma_{\rm EC} = 2.90 \ {\rm pc} \qquad z_{\rm T} = 520 \ {\rm pc} \qquad z_{\rm T} = 520 \ {\rm pc} \qquad z_{\rm T} = 500 \ {\rm pc} \\ z_{\rm T} = 520 \ {\rm pc} \qquad z_{\rm T} = 500 \ {\rm pc} \qquad z_{\rm T} = 500 \ {\rm pc} \\ z_{\rm T} = 5.0 \ {\rm pc} \qquad z_{\rm T} = 500 \ {\rm pc} \qquad z_{\rm T} = 500 \ {\rm pc} \\ z_{\rm T} = 5.0 \ {\rm pc} \qquad z_{\rm T} = 500 \ {\rm pc} \qquad z_{\rm T} = 500 \ {\rm pc} \\ z_{\rm T} = 110 \ {\rm pc} \qquad z_{\rm T} = 520 \ {\rm pc} \qquad z_{\rm T} = 500 \ {\rm pc} \\ z_{\rm T} = 520 \ {\rm pc} \qquad z_{\rm T} = 500 \ {\rm pc} \qquad z_{\rm EC} = 2470 \ {\rm pc} \\ 0.5 r_{25} < R < 0.8 r_{25} \qquad \mu_1 = 25.67 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \rho_{\rm T0}/\rho_{\rm 00} = 0.39 \qquad \rho_{\rm T0}/\rho_{\rm 00} = 0.70 \\ \rho_{\rm T0}/\rho_{\rm 00} = 0.39 \qquad \rho_{\rm T0}/\rho_{\rm 00} = 0.70 \\ \rho_{\rm T0}/\rho_{\rm 00} = 5.57 \qquad \rho_{\rm T0}/\rho_{\rm 00} = 0.70 \\ \rho_{\rm T0}/\rho_{\rm 00} = 5.57 \qquad \rho_{\rm T0}/\rho_{\rm 00} = 0.70 \\ \sigma_{\rm T}/\sigma_{\rm t} = 2.35 \qquad \sigma_{\rm T}/\sigma_{\rm t} = 2.50 \ {\rm pc} \qquad z_{\rm T} = 5.00 \ {\rm pc} \\ z_{\rm T} = 1.19 \qquad \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.48 \ z_{\rm T}/\Sigma_{\rm E} = 1.19 \qquad \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.48 \ z_{\rm t} = 150 \ {\rm pc} \qquad z_{\rm t} = 550 \ {\rm pc} \ z_{\rm t} = 150 \ {\rm pc} \qquad z_{\rm t} = 550 \ {\rm pc} \ z_{\rm t} = 1500 \ {\rm pc} \ z_{\rm t} = 1500 \ {\rm pc} \ $			
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$\begin{split} & \Sigma_{T}/\Sigma_{t} = 1.19 \qquad \Sigma_{T}/\Sigma_{t} = 2.13 \\ & \Sigma_{T}/\Sigma_{EC} = 2.91 \qquad \Sigma_{T}/\Sigma_{EC} = 3.02 \\ & z_{t} = 110 \ \text{pc} \qquad z_{t} = 110 \ \text{pc} \\ & z_{T} = 510 \ \text{pc} \qquad z_{T} = 530 \ \text{pc} \\ & z_{EC} = 2780 \ \text{pc} \qquad z_{EC} = 2890 \ \text{pc} \\ \hline 0.2 \ r_{25} < R < 0.5 \ r_{25} \qquad \mu_{1} = 25.93 \ \text{mag} \ \text{arcsec}^{-2} \\ & \Delta m = 7.5 \ \text{mag} \ \text{arcsec}^{-2} \\ & \Delta m = 7.5 \ \text{mag} \ \text{arcsec}^{-2} \\ & \rho_{T0}/\rho_{t0} = 0.35 \qquad \rho_{T0}/\rho_{t0} = 0.64 \\ & \rho_{T0}/\rho_{EC0} = 11.60 \qquad \rho_{T0}/\rho_{EC0} = 10.60 \\ & \sigma_{T}/\sigma_{t} = 2.60 \qquad \sigma_{T}/\sigma_{t} = 2.69 \\ & \sigma_{T}/\sigma_{EC} = 0.44 \qquad \sigma_{T}/\sigma_{EC} = 0.43 \\ & \Sigma_{T}/\Sigma_{t} = 1.25 \qquad \Sigma_{T}/\Sigma_{t} = 2.25 \\ & \Sigma_{T}/\Sigma_{EC} = 3.13 \qquad \Sigma_{T}/\Sigma_{EC} = 2.94 \\ & z_{t} = 110 \ \text{pc} \qquad z_{T} = 500 \ \text{pc} \\ & z_{EC} = 2540 \ \text{pc} \qquad z_{EC} = 2470 \ \text{pc} \\ \hline 0.5 \ r_{25} < R < 0.8 \ r_{25} \qquad \mu_{1} = 25.67 \ \text{mag} \ \text{arcsec}^{-2} \\ & \rho_{T0}/\rho_{t0} = 0.39 \qquad \rho_{T0}/\rho_{t0} = 0.70 \\ & \rho_{T0}/\rho_{t0} = 0.39 \qquad \rho_{T0}/\rho_{t0} = 0.70 \\ & \rho_{T0}/\rho_{t0} = 0.39 \qquad \rho_{T0}/\rho_{t0} = 0.70 \\ & \rho_{T0}/\rho_{t0} = 0.39 \qquad \rho_{T0}/\rho_{t0} = 5.00 \\ & \sigma_{T}/\sigma_{t} = 2.35 \qquad \sigma_{T}/\sigma_{t} = 2.50 \\ & \sigma_{T}/\sigma_{t} = 2.35 \qquad \sigma_{T}/\sigma_{t} = 2.50 \\ & \sigma_{T}/\sigma_{EC} = 0.44 \qquad \sigma_{T}/\sigma_{EC} = 0.44 \\ & \Sigma_{T}/\Sigma_{t} = 1.19 \qquad \Sigma_{T}/\Sigma_{t} = 2.19 \\ & \Sigma_{T}/\Sigma_{EC} = 1.58 \qquad \Sigma_{T}/\Sigma_{EC} = 1.48 \\ & z_{t} = 150 \ \text{pc} \qquad z_{T} = 590 \ \text{pc} \\ & z_{T} = 620 \ \text{pc} \qquad z_{T} = 590 \ \text{pc} \\ & z_{T} = 50 \ \text{pc} \\ & z_{T} = 500 \ \text{pc} \\ & z_{T} = 500 \ p$			
$\begin{split} & \sum_{T_{1}} \sum_{EC} = 2.91 \qquad \sum_{T_{1}} \sum_{EC} = 3.02 \\ z_{t} = 110 \ \text{pc} \qquad z_{T} = 530 \ \text{pc} \\ z_{EC} = 2780 \ \text{pc} \qquad z_{EC} = 2890 \ \text{pc} \\ \hline \\ \hline 0.2 \ r_{25} < R < 0.5 \ r_{25} \qquad & \mu_{1} = 25.93 \ \text{mg} \ \text{arcsec}^{-2} \\ & \Delta m = 7.5 \ \text{mg} \ \text{arcsec}^{-2} \\ & \Delta m = 7.5 \ \text{mg} \ \text{arcsec}^{-2} \\ & \rho_{T0} / \rho_{t0} = 0.35 \qquad \rho_{T0} / \rho_{t0} = 0.64 \\ & \rho_{T0} / \rho_{EC} = 11.60 \qquad \rho_{T0} / \rho_{EC} = 10.60 \\ & \sigma_{T} / \sigma_{EC} = 0.44 \qquad \sigma_{T} / \sigma_{EC} = 0.43 \\ & \Sigma_{T} / \Sigma_{EC} = 3.13 \qquad \Sigma_{T} / \Sigma_{EC} = 2.94 \\ & z_{t} = 110 \ \text{pc} \qquad z_{T} = 500 \ \text{pc} \\ & z_{T} = 520 \ \text{pc} \qquad z_{T} = 500 \ \text{pc} \\ & z_{EC} = 2540 \ \text{pc} \qquad z_{EC} = 2470 \ \text{pc} \\ \hline 0.5 \ r_{25} < R < 0.8 \ r_{25} \qquad & \mu_{1} = 25.67 \ \text{mg} \ \text{arcsec}^{-2} \\ & \Delta m = 5.5 \ \text{mg} \ \text{arcsec}^{-2} \\ & \rho_{T0} / \rho_{t0} = 0.39 \qquad \rho_{T0} / \rho_{t0} = 0.70 \\ & \rho_{T0} / \rho_{EC} = 5.57 \qquad \rho_{T0} / \rho_{EC} = 5.00 \\ & \sigma_{T} / \sigma_{EC} = 0.44 \qquad \sigma_{T} / \sigma_{EC} = 0.44 \\ & \Sigma_{T} / \Sigma_{t} = 1.19 \qquad \Sigma_{T} / \Sigma_{t} = 2.50 \\ & \sigma_{T} / \sigma_{EC} = 0.44 \qquad \sigma_{T} / \sigma_{EC} = 0.44 \\ & \Sigma_{T} / \Sigma_{t} = 1.19 \qquad \Sigma_{T} / \Sigma_{t} = 2.19 \\ & \Sigma_{T} / \Sigma_{EC} = 1.58 \qquad \Sigma_{T} / \Sigma_{EC} = 1.48 \\ & z_{t} = 150 \ \text{pc} \qquad z_{T} = 590 \ \text{pc} \\ & z_{T} = 620 \ \text{pc} \qquad z_{T} = 590 \ \text{pc} \\ & z_{T} = 500 \ \text{pc} \\ & z_{T} = 5$			
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$\begin{array}{c c} z_{\rm T} = 510 \ {\rm pc} & z_{\rm T} = 530 \ {\rm pc} \\ z_{\rm EC} = 2780 \ {\rm pc} & z_{\rm EC} = 2890 \ {\rm pc} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} 0.2 \ r_{25} < R < 0.5 \ r_{25} & \mu_1 = 25.93 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 7.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \rho_{\rm T0} / \rho_{00} = 0.35 & \rho_{\rm T0} / \rho_{10} = 0.64 \\ \rho_{\rm T0} / \rho_{\rm EC} = 11.60 & \rho_{\rm T0} / \rho_{\rm EC0} = 10.60 \\ \sigma_{\rm T} / \sigma_{\rm EC} = 0.44 & \sigma_{\rm T} / \sigma_{\rm EC} = 0.43 \\ \Sigma_{\rm T} / \Sigma_{\rm EC} = 3.13 & \Sigma_{\rm T} / \Sigma_{\rm EC} = 2.94 \\ z_{\rm t} = 110 \ {\rm pc} & z_{\rm t} = 100 \ {\rm pc} \\ z_{\rm T} = 520 \ {\rm pc} & z_{\rm T} = 500 \ {\rm pc} \\ z_{\rm EC} = 2540 \ {\rm pc} & z_{\rm EC} = 2470 \ {\rm pc} \\ \hline \end{array} \\ \hline \hline \begin{array}{c} 0.5 \ r_{25} < R < 0.8 \ r_{25} & \mu_1 = 25.67 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 5.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \rho_{\rm T0} / \rho_{\rm t0} = 0.39 & \rho_{\rm T0} / \rho_{\rm t0} = 0.70 \\ \rho_{\rm T0} / \rho_{\rm EC0} = 5.57 & \rho_{\rm T0} / \rho_{\rm EC0} = 5.00 \\ \sigma_{\rm T} / \sigma_{\rm t} = 2.35 & \sigma_{\rm T} / \sigma_{\rm t} = 2.50 \\ \sigma_{\rm T} / \sigma_{\rm t} = 2.35 & \sigma_{\rm T} / \sigma_{\rm t} = 2.50 \\ \sigma_{\rm T} / \sigma_{\rm t} = 2.35 & \sigma_{\rm T} / \sigma_{\rm t} = 2.50 \\ \sigma_{\rm T} / \sigma_{\rm t} = 2.35 & \sigma_{\rm T} / \sigma_{\rm t} = 2.50 \\ \sigma_{\rm T} / \sigma_{\rm t} = 1.19 & \Sigma_{\rm T} / \Sigma_{\rm t} = 2.19 \\ \Sigma_{\rm T} / \Sigma_{\rm t} = 1.19 & \Sigma_{\rm T} / \Sigma_{\rm t} = 2.19 \\ \Sigma_{\rm T} / \Sigma_{\rm EC} = 1.58 & \Sigma_{\rm T} / \Sigma_{\rm EC} = 1.48 \\ z_{\rm t} = 150 \ {\rm pc} & z_{\rm T} = 590 \ {\rm pc} \\ z_{\rm T} = 620 \ {\rm pc} & z_{\rm T} = 590 \ {\rm pc} \\ \end{array}$		-,	-,
$\frac{z_{\rm EC} = 2780 \text{ pc}}{0.2 r_{25} < R < 0.5 r_{25}} \qquad \begin{array}{c} \mu_1 = 25.93 \text{ mg arcsec}^{-2} \\ \Delta m = 7.5 \text{ mg arcsec}^{-2} \\ \rho_{\rm T0}/\rho_{0} = 0.35 & \rho_{\rm T0}/\rho_{0} = 0.64 \\ \rho_{\rm T0}/\rho_{\rm EC} = 11.60 & \rho_{\rm T0}/\rho_{\rm EC0} = 10.60 \\ \sigma_{\rm T}/\sigma_{\rm t} = 2.60 & \sigma_{\rm T}/\sigma_{\rm t} = 2.69 \\ \sigma_{\rm T}/\sigma_{\rm tC} = 0.44 & \sigma_{\rm T}/\sigma_{\rm EC} = 0.43 \\ \Sigma_{\rm T}/\Sigma_{\rm t} = 1.25 & \Sigma_{\rm T}/\Sigma_{\rm EC} = 2.94 \\ z_{\rm t} = 110 \text{ pc} & z_{\rm t} = 100 \text{ pc} \\ z_{\rm T} = 520 \text{ pc} & z_{\rm T} = 500 \text{ pc} \\ z_{\rm EC} = 2540 \text{ pc} & z_{\rm EC} = 2470 \text{ pc} \\ \hline 0.5 r_{25} < R < 0.8 r_{25} & \mu_1 = 25.67 \text{ mg arcsec}^{-2} \\ \rho_{\rm T0}/\rho_{10} = 0.39 & \rho_{\rm T0}/\rho_{10} = 0.70 \\ \rho_{\rm T0}/\rho_{\rm EC0} = 5.57 & \rho_{\rm T0}/\rho_{\rm EC0} = 5.00 \\ \sigma_{\rm T}/\sigma_{\rm t} = 2.35 & \sigma_{\rm T}/\sigma_{\rm t} = 2.50 \\ \sigma_{\rm T}/\sigma_{\rm t} = 2.35 & \sigma_{\rm T}/\sigma_{\rm t} = 2.50 \\ \sigma_{\rm T}/\sigma_{\rm t} = 2.35 & \sigma_{\rm T}/\sigma_{\rm t} = 2.50 \\ \sigma_{\rm T}/\sigma_{\rm t} = 2.35 & \sigma_{\rm T}/\sigma_{\rm t} = 2.50 \\ \sigma_{\rm T}/\sigma_{\rm t} = 2.35 & \sigma_{\rm T}/\sigma_{\rm t} = 2.50 \\ \sigma_{\rm T}/\sigma_{\rm EC} = 0.44 & \sigma_{\rm T}/\sigma_{\rm EC} = 0.44 \\ \Sigma_{\rm T}/\Sigma_{\rm t} = 1.19 & \Sigma_{\rm T}/\Sigma_{\rm t} = 2.19 \\ \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.58 & \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.48 \\ z_{\rm t} = 150 \text{ pc} & z_{\rm T} = 590 \text{ pc} \\ z_{\rm T} = 620 \text{ pc} & z_{\rm T} = 590 \text{ pc} \\ \end{array}$			· •
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$		$\rho_{\rm T0}/\rho_{\rm t0} = 0.35$	$\rho_{\rm T0}/\rho_{\rm t0} = 0.64$
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$\begin{split} & \sum_{T} / \Sigma_{EC} = 3.13 \qquad \sum_{T} / \Sigma_{EC} = 2.94 \\ & z_t = 110 \ \text{pc} \qquad z_t = 100 \ \text{pc} \\ & z_T = 520 \ \text{pc} \qquad z_T = 500 \ \text{pc} \\ & z_{EC} = 2540 \ \text{pc} \qquad z_{EC} = 2470 \ \text{pc} \\ \hline & 0.5 \ r_{25} < R < 0.8 \ r_{25} \qquad \mu_1 = 25.67 \ \text{mag} \ \text{arcsec}^{-2} \\ & \Delta m = 5.5 \ \text{mag} \ \text{arcsec}^{-2} \\ & \rho_{T0} / \rho_{t0} = 0.39 \qquad \rho_{T0} / \rho_{t0} = 0.70 \\ & \rho_{T0} / \rho_{EC0} = 5.57 \qquad \rho_{T0} / \rho_{EC0} = 5.00 \\ & \sigma_T / \sigma_t = 2.35 \qquad \sigma_T / \sigma_t = 2.50 \\ & \sigma_T / \sigma_{EC} = 0.44 \qquad \sigma_T / \sigma_{EC} = 0.44 \\ & \Sigma_T / \Sigma_t = 1.19 \qquad \Sigma_T / \Sigma_t = 2.19 \\ & \Sigma_T / \Sigma_{EC} = 1.58 \qquad \Sigma_T / \Sigma_{EC} = 1.48 \\ & z_t = 150 \ \text{pc} \qquad z_T = 590 \ \text{pc} \\ \hline \end{cases}$			
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$ \begin{array}{c c} z_{\rm EC} = 2540 \ {\rm pc} & z_{\rm EC} = 2470 \ {\rm pc} \\ \hline \\ z_{\rm EC} = 2540 \ {\rm pc} & z_{\rm EC} = 2470 \ {\rm pc} \\ \hline \\ \mu_1 = 25.67 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \Delta m = 5.5 \ {\rm mag} \ {\rm arcsec}^{-2} \\ \hline \\ \rho_{\rm T0}/\rho_{\rm t0} = 0.39 & \rho_{\rm T0}/\rho_{\rm t0} = 0.70 \\ \hline \\ \rho_{\rm T0}/\rho_{\rm EC0} = 5.57 & \rho_{\rm T0}/\rho_{\rm EC0} = 5.00 \\ \hline \\ \sigma_{\rm T}/\sigma_{\rm t} = 2.35 & \sigma_{\rm T}/\sigma_{\rm t} = 2.50 \\ \hline \\ \sigma_{\rm T}/\sigma_{\rm EC} = 0.44 & \sigma_{\rm T}/\sigma_{\rm EC} = 0.44 \\ \hline \\ \Sigma_{\rm T}/\Sigma_{\rm t} = 1.19 & \Sigma_{\rm T}/\Sigma_{\rm t} = 2.19 \\ \hline \\ \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.58 & \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.48 \\ z_{\rm t} = 150 \ {\rm pc} & z_{\rm T} = 590 \ {\rm pc} \\ \hline \end{array} $			
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$\Delta m = 5.5 \text{ mag arcsec}^{-2}$ $\rho_{T0}/\rho_{t0} = 0.39 \qquad \rho_{T0}/\rho_{t0} = 0.70$ $\rho_{T0}/\rho_{EC0} = 5.57 \qquad \rho_{T0}/\rho_{EC0} = 5.00$ $\sigma_{T}/\sigma_{t} = 2.35 \qquad \sigma_{T}/\sigma_{t} = 2.50$ $\sigma_{T}/\sigma_{EC} = 0.44 \qquad \sigma_{T}/\sigma_{EC} = 0.44$ $\Sigma_{T}/\Sigma_{t} = 1.19 \qquad \Sigma_{T}/\Sigma_{t} = 2.19$ $\Sigma_{T}/\Sigma_{EC} = 1.58 \qquad \Sigma_{T}/\Sigma_{EC} = 1.48$ $z_{t} = 150 \text{ pc} \qquad z_{t} = 150 \text{ pc}$ $z_{T} = 620 \text{ pc} \qquad z_{T} = 590 \text{ pc}$		$z_{\rm EC} = 2540 \ {\rm pc}$	$z_{\rm EC} = 2470 {\rm pc}$
$\begin{array}{lll} \rho_{T0}/\rho_{t0} = 0.39 & \rho_{T0}/\rho_{t0} = 0.70 \\ \rho_{T0}/\rho_{EC0} = 5.57 & \rho_{T0}/\rho_{EC0} = 5.00 \\ \sigma_{T}/\sigma_{t} = 2.35 & \sigma_{T}/\sigma_{t} = 2.50 \\ \sigma_{T}/\sigma_{EC} = 0.44 & \sigma_{T}/\sigma_{EC} = 0.44 \\ \Sigma_{T}/\Sigma_{t} = 1.19 & \Sigma_{T}/\Sigma_{t} = 2.19 \\ \Sigma_{T}/\Sigma_{EC} = 1.58 & \Sigma_{T}/\Sigma_{EC} = 1.48 \\ z_{t} = 150 \ \text{pc} & z_{t} = 150 \ \text{pc} \\ z_{T} = 620 \ \text{pc} & z_{T} = 590 \ \text{pc} \end{array}$	$0.5 r_{25} < R < 0.8 r_{25}$		
$\begin{array}{ll} \rho_{\rm T0}/\rho_{\rm EC0} = 5.57 & \rho_{\rm T0}/\rho_{\rm EC0} = 5.00 \\ \sigma_{\rm T}/\sigma_{\rm t} = 2.35 & \sigma_{\rm T}/\sigma_{\rm t} = 2.50 \\ \sigma_{\rm T}/\sigma_{\rm EC} = 0.44 & \sigma_{\rm T}/\sigma_{\rm EC} = 0.44 \\ \Sigma_{\rm T}/\Sigma_{\rm t} = 1.19 & \Sigma_{\rm T}/\Sigma_{\rm t} = 2.19 \\ \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.58 & \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.48 \\ z_{\rm t} = 150 \ {\rm pc} & z_{\rm t} = 150 \ {\rm pc} \\ z_{\rm T} = 620 \ {\rm pc} & z_{\rm T} = 590 \ {\rm pc} \end{array}$			
$\begin{aligned} \sigma_{\rm T} / \sigma_{\rm t} &= 2.35 & \sigma_{\rm T} / \sigma_{\rm t} &= 2.50 \\ \sigma_{\rm T} / \sigma_{\rm EC} &= 0.44 & \sigma_{\rm T} / \sigma_{\rm EC} &= 0.44 \\ \Sigma_{\rm T} / \Sigma_{\rm t} &= 1.19 & \Sigma_{\rm T} / \Sigma_{\rm t} &= 2.19 \\ \Sigma_{\rm T} / \Sigma_{\rm EC} &= 1.58 & \Sigma_{\rm T} / \Sigma_{\rm EC} &= 1.48 \\ z_t &= 150 \ {\rm pc} & z_t &= 150 \ {\rm pc} \\ z_{\rm T} &= 620 \ {\rm pc} & z_{\rm T} &= 590 \ {\rm pc} \end{aligned}$			
$ \begin{array}{ll} \sigma_{\rm T}/\sigma_{\rm EC} = 0.44 & \sigma_{\rm T}/\sigma_{\rm EC} = 0.44 \\ \Sigma_{\rm T}/\Sigma_t = 1.19 & \Sigma_{\rm T}/\Sigma_t = 2.19 \\ \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.58 & \Sigma_{\rm T}/\Sigma_{\rm EC} = 1.48 \\ z_t = 150 \ {\rm pc} & z_t = 150 \ {\rm pc} \\ z_{\rm T} = 620 \ {\rm pc} & z_{\rm T} = 590 \ {\rm pc} \end{array} $			
$\begin{split} \Sigma_{\rm T} / \Sigma_{\rm t} &= 1.19 & \Sigma_{\rm T} / \Sigma_{\rm t} &= 2.19 \\ \Sigma_{\rm T} / \Sigma_{\rm EC} &= 1.58 & \Sigma_{\rm T} / \Sigma_{\rm EC} &= 1.48 \\ z_{\rm t} &= 150 \ {\rm pc} & z_{\rm t} &= 150 \ {\rm pc} \\ z_{\rm T} &= 620 \ {\rm pc} & z_{\rm T} &= 590 \ {\rm pc} \end{split}$		-, -	-, -
$\begin{array}{ll} \Sigma_{\rm T} / \Sigma_{\rm EC} = 1.58 & \Sigma_{\rm T} / \Sigma_{\rm EC} = 1.48 \\ z_{\rm t} = 150 \ {\rm pc} & z_{\rm t} = 150 \ {\rm pc} \\ z_{\rm T} = 620 \ {\rm pc} & z_{\rm T} = 590 \ {\rm pc} \end{array}$		-,	-,
$z_t = 150 \text{ pc}$ $z_t = 150 \text{ pc}$ $z_T = 620 \text{ pc}$ $z_T = 590 \text{ pc}$			
$z_{\rm T} = 620 \ {\rm pc}$ $z_{\rm T} = 590 \ {\rm pc}$, .
* *			
$z_{\text{EC}} = 2000 \text{ bc} \qquad z_{\text{EC}} = 2700 \text{ bc}$		*	
		$z_{\rm EC} = 2000 \rm pc$	$z_{\rm EC} = 2700 \rm pc$

Notes. Υ_T/Υ_t : ratio of the thick and thin disk mass-to-light ratios; μ_1 : limiting magnitude of the fit; Δm : dynamical range over which the fit has been produced; ρ_{T0}/ρ_{t0} , ρ_{T0}/ρ_{EC0} : midplane thick-to-thin and thick-to-EC mass density ratios; σ_T/σ_t , σ_T/σ_{EC} : thick-to-thin and thick-to-EC vertical velocity dispersion ratios; Σ_T/Σ_t , Σ_T/Σ_{EC} : thick-to-thin and thick-to-EC stellar column mass density ratios; z_t , z_T , z_{EC} : thin, thick, and EC scale heights.

for $0.2r_{25} < |R| < 0.5r_{25}$ is significantly higher (a factor of two) than it is for $0.5r_{25} < |R| < 0.8r_{25}$ implying that the scale length is significantly larger than that of the thin and the thick disk.

Using the weightings in Equation (5) from CO11b, we find that the ratios of masses of the stellar components are $M_T/M_t =$ 1.22 ($M_T/M_t = 2.19$) and $M_T/M_{EC} = 2.74$ ($M_T/M_{EC} = 2.69$) for $\Upsilon_T/\Upsilon_t = 1.2$ ($\Upsilon_T/\Upsilon_t = 2.4$). When taking the mass of the thick disk and the EC together ($M_T + M_{EC}$)/ $M_t = 1.67$ (($M_T + M_{EC}$)/ $M_t = 3.00$). With a circular velocity speed of

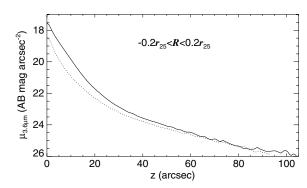


Figure 4. Luminosity profile for the $-0.2r_{25} < R < 0.2r_{25}$ bin (solid line) compared to that obtained from the $0.2r_{25} < |R| < 0.5r_{25}$ bins (dotted line).

 $v_c = 181.7 \text{ km s}^{-1}$ (HyperLEDA), NGC 4013 would not fit in the M_T/M_t-v_c relationship discovered by Yoachim & Dalcanton (2006) and shown in Figure 12 of CO11b both when considering M_T/M_t and $(M_T + M_{EC})/M_t$. Furthermore, if we consider the thick disk as part of the thin disk and the EC to be the only thick disk in NGC 4013, we get $M_{EC}/(M_t + M_T) = 0.20$ $(M_{EC}/(M_t + M_T) = 0.26)$, which is too low to fit into the M_T/M_t-v_c relationship.

The luminosity profiles could not be satisfactorily fitted by a sum of two sech²(z/z_0) functions, but were acceptably fitted by a sum of two exponential functions. The $\sqrt{(\chi^2)}$ was, however, worse than in the three-disk fit and misses a substantial amount of light corresponding to the thinner component of the three-disk fit (0.2–0.3 mag arcsec⁻² for the inner bins). This fit, although simpler than that made with three coupled stellar components, should be regarded as unphysical.

4. DISCUSSION

Just as causal links have been sought between the "prodigious" warp and the merging event causing the "giant" stream, one may also be tempted to find links between a minor merger and the EC of NGC 4013.

If the EC is linked to the minor merger, then it can be made of tidal debris. According to the images in MD09, the tidal loops should not affect the luminosity profiles at R = 0. Although producing a fit for the minor axis using our procedure is impossible due to the presence of the bulge, we produced the luminosity profile (Figure 4). It is clear that in the bin with $-0.2 r_{25} < R < 0.2 r_{25}$ the EC is present and probably slightly brighter than in the $0.2 r_{25} < |R| < 0.5 r_{25}$ as predicted in the case of a disk or an ellipsoid. The color analysis made by MD09 shows that the tidal stream is much redder than the EC, although the large error bars make a common origin still possible. Other arguments against a tidal origin for the EC are its smoothness, its symmetry, and the uniformity of its scale height with varying radial distance *R*.

Another possibility is that the EC has been formed by the dynamical heating of the disks by the crossing of the dwarf galaxy causing the tidal stream. However, as the disk self-gravity which counteracts the disk heating is higher at low galactocentric radii, disks formed in this way appear flared and, as a consequence, the EC would form with a relatively small scale height at low *R*. Simulations (Quinn et al. 1993; Walker et al. 1996; Kazantzidis et al. 2008; Bournaud et al. 2009) show how this mechanism could reasonably produce the observed scale heights at high galactocentric radius, but would fail to produce such an EC for the inner kiloparsecs. Additionally, it

seems difficult to create a component containing 20% (26%) of the mass of the galaxy if we assume $\Upsilon_T/\Upsilon_t = 1.2 (\Upsilon_T/\Upsilon_t = 2.4)$ in a recent event without disturbing the disks. The regularity and the symmetry of the galaxy argue for an old origin for the EC, thus confirming that the assumption of equilibrium is reasonable. Finally, the stream in NGC 4013 is Monoceroslike (MD09), thus probably a very minor merger (~1:100; Peñarrubia et al. 2005) not likely to cause large disturbances. The possibility of the EC being created during an older merger event cannot be discarded; Purcell et al. (2010) have shown that a 1:10 merger 5 Gyr ago in a Milky Way like galaxy yields results which qualitatively match the appearance of NGC 4013 except for the fact that their resulting EC is more boxy than the one we detect and we do not find the same flaring. They show that low-latitude accretion events could heat up to 1% of the disk mass to z > 7 kpc, which is in rough agreement with what we found (1.8% of disk mass at z > 7 kpc).

We also discard the EC to be the effect of a stellar warp seen in projection. Bottema (1995) found that the stellar disk is truncated at the radius at which the warp starts and the warp model made by Bottema (1996) shows that its line of nodes is in the direction of the line of sight, making a stellar warp look as a thick disk when seen in projection impossible. Even if the H I warp and the stellar warp were decoupled and with different lines of nodes the stellar warp would be unlikely to mimic an EC unless the stellar warp started at a radius smaller than the H I warp.

Thus, we deduce from our findings and from literature data that the EC is a real feature and not some tidal feature or warp seen in projection. We also deduce that both the thick disk and the EC are old. A possible scenario for the formation of a three-component system would be having a disk formed thick with stars formed before and during the buildup of the galaxy from small fragments (Robertson et al. 2006; Brook et al. 2007; Richard et al. 2010) and/or a disk heated by the internal thickening caused by kinematical heating due to giant clumps (Elmegreen & Elmegreen 2006). Then a merger event would further thicken the disk, which would become what we know as the EC. After the merger, the canonical thick disk would form with the same mechanisms as the EC formed prior to the merger event. Finally, the remaining gas, plus that coming from cold flows would settle in the midplane and form the thin disk. This disk formation mechanism is not very frequent, since only 2 galaxies over 46 exhibit a bright EC in CO11b. The difference in the formation mechanisms may explain why these two galaxies fall outside the M_T/M_t - v_c relationship discovered by Yoachim & Dalcanton (2006).

5. CONCLUSIONS

NGC 4013 is not adequately described by the canonical thin+thick disk description (CO11b). In this Letter, the luminosity profiles of NGC 4013 are fitted satisfactorily using the solutions of three stellar flattened components plus one gaseous disk in equilibrium. The newly described extended component (EC) has a relatively low surface brightness, but due to its vertical extent, contains a significant fraction of the disk mass (between 20% and 26% depending on the assumed Υ_t/Υ_T). The EC has a longer scale length than the galaxy disks, is smooth, and its properties do not depend strongly on varying galactocentric radii.

The nature of the EC is unknown and could be a second thick disk or a squashed elliptical halo. The smoothness of the EC makes it unlikely to be related to the ongoing minor merger of NGC 4013. We also discard the EC to be made of off-plane stars of a warped disk, since the warp has been modeled to have its line of nodes in the direction of the line of sight (Bottema 1996). We favor a scenario in which the EC was formed in a two-stage process, in which an initially thick disk was dynamically heated by a merger soon enough in the galaxy history to have a new thick disk formed within it.

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